

(12) UK Patent Application (19) GB (11) 2 246 713 (13) A

(43) Date of A publication 12.02.1992

(21) Application No 9116326.1

(22) Date of filing 29.07.1991

(30) Priority data
(31) 558468 (32) 27.07.1990 (33) US

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(51) INT CL⁶
A61M 1/34

(52) UK CL (Edition K)
B1D DNMB
U1S S1296

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EP 0267286 A1 EP 0155003 A2 US 4046696 A

(58) Field of search
UK CL (Edition K) B1D DBFA DBGA DBHA DCEA
DNMB DNRJ
INT CL⁶ A61M 1/34, B01D 39/04 39/16

(54) Leucocyte depleting filter

(57) Blood is filtered at more than 25 millilitres per minute to reduce the leucocyte content through a filter housing having a tangential inlet, an inward flow annular filter element 52 comprising a mass of polymeric fibres with a CWS7 over 52 dynes/cm and an air vent 30 separated from the rest of the filter by a liquid-repelling porous membrane 31. Blood passes from the inlet to element 52 through a preliminary foam plastic filter element 50, which coalesces any air bubbles to facilitate separation. The filter is used in conjunction with an artificial lung, during open heart surgery.

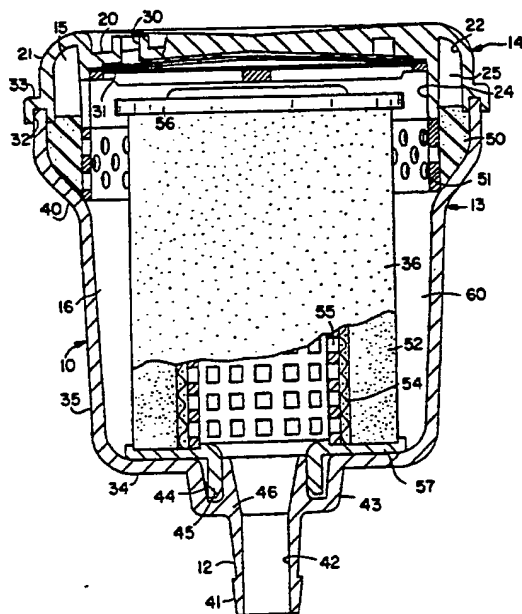


FIG. 1

At least one drawing originally filed was informal and the print reproduced here is taken from a later filed formal copy.

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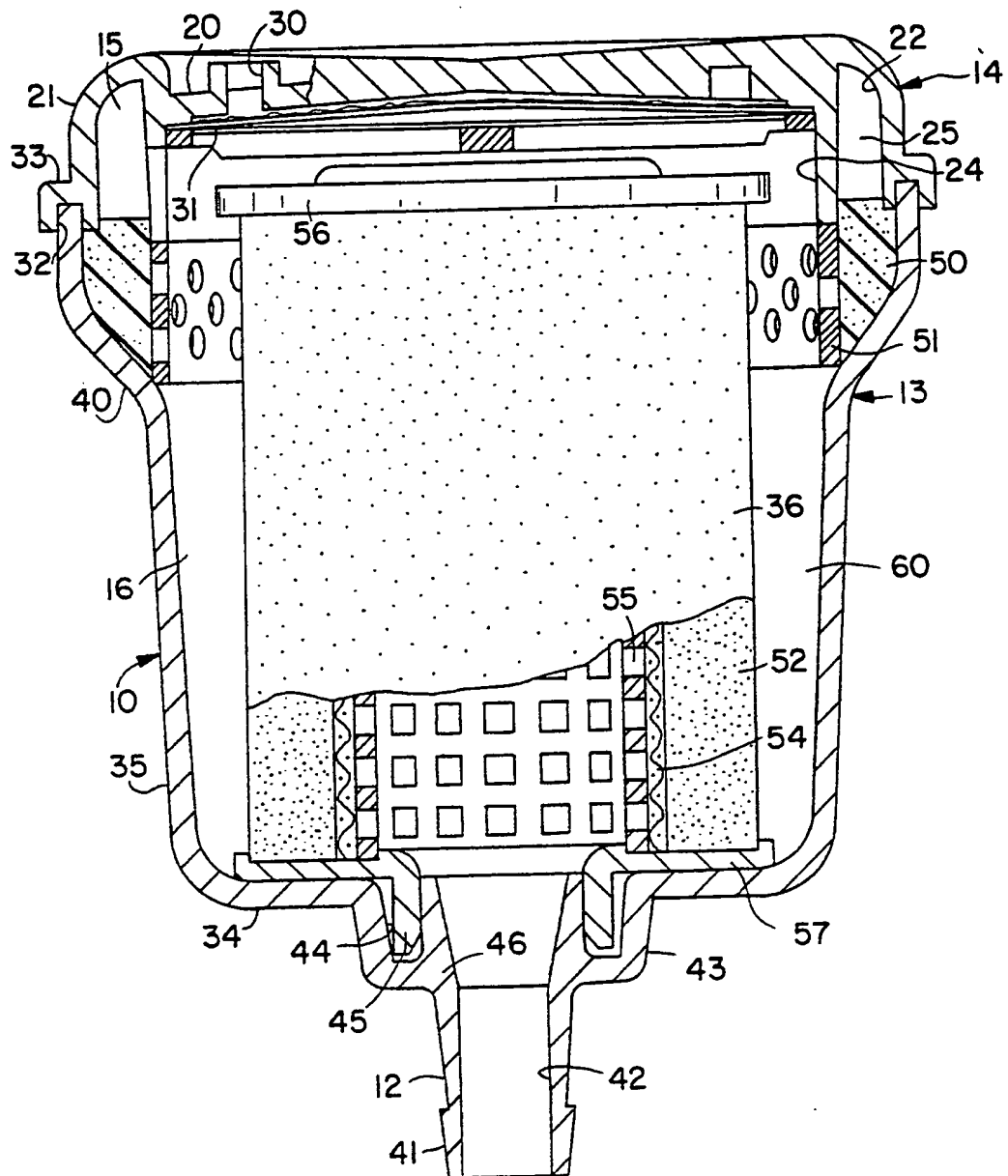


FIG. 1

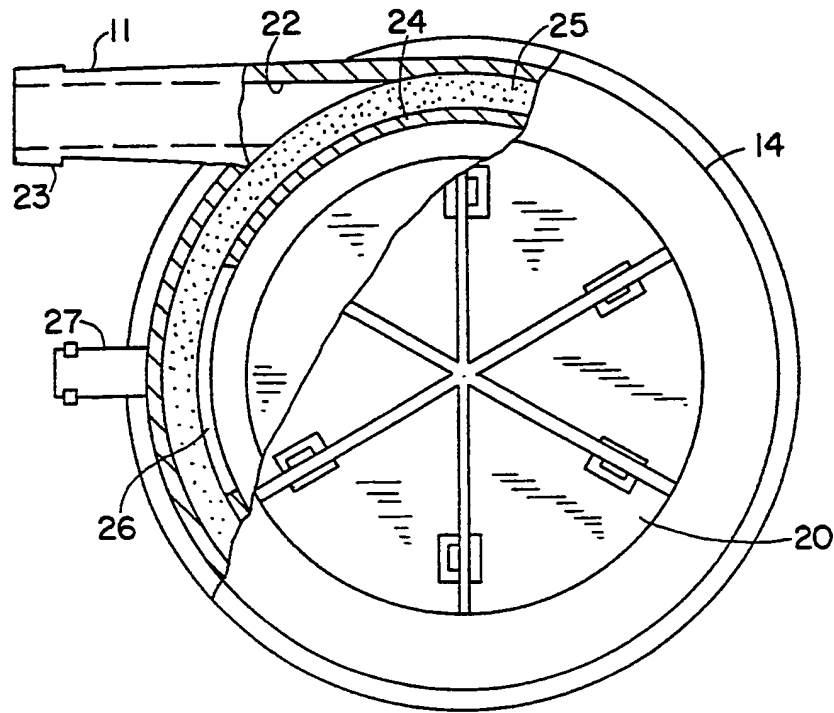


FIG. 2

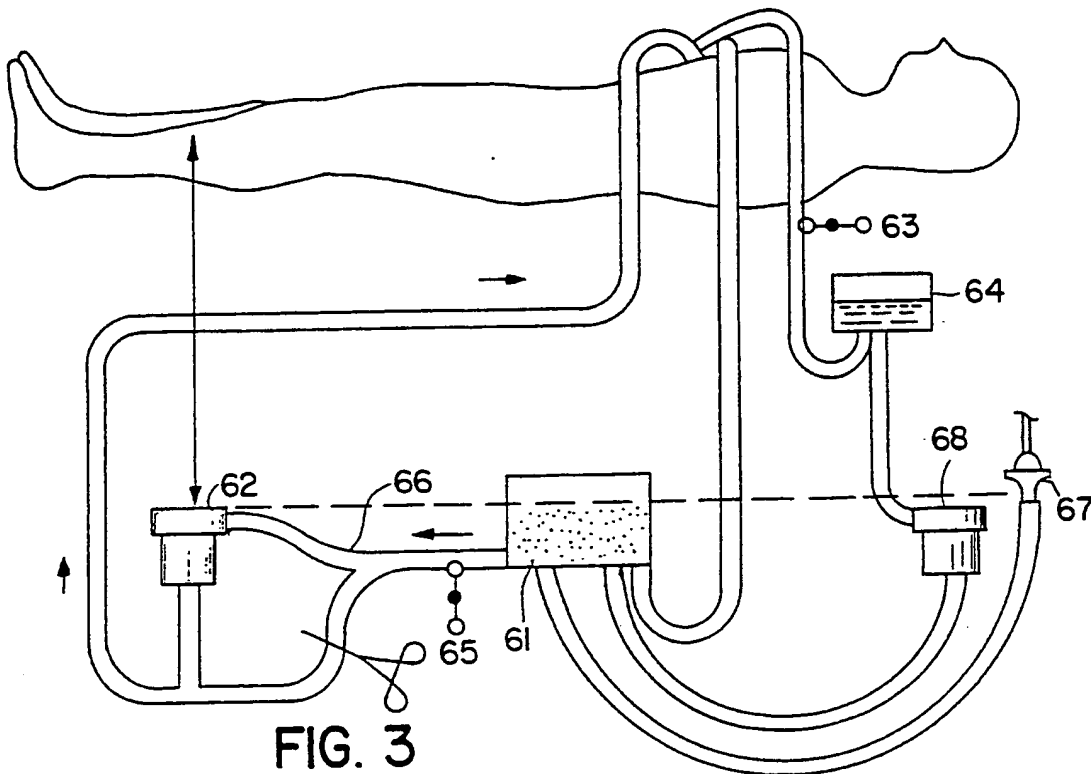


FIG. 3

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LEUCOCYTE DEPLETING FILTER DEVICE AND METHOD OF USE

The invention relates to filter devices for removing leucocytes and other deleterious material from leucocyte-containing liquids such as blood.

5 For example, the invention relates to the removal of leucocytes from blood in an extracorporeal circuit.

Patients undergoing open heart surgery have the pumping functions of the heart and the gas exchange functions of the lungs temporarily replaced by
10 various apparatus in an external (extracorporeal) circuit. In the last 30 years, technological advances related to the components of these extracorporeal systems have provided significant benefits to these patients. For example, completely
15 disposable components of an extracorporeal circuit and associated blood-contacting surfaces have been fabricated, which eliminate adverse patient reactions due to contamination from trace amounts of a previous patient's blood supply.

20 During a typical operation requiring extracorporeal circulation, blood from the cardiovascular system of the patient is typically taken from the patient and delivered through tubing to an oxygenator which serves as an external lung.
25 Within the oxygenator, blood is exposed to an appropriate percentage of oxygen and carbon dioxide. The perfusate is drawn from the oxygenator by an arterial pump and delivered to a blood filter, which removes gaseous microemboli, fat emboli, aggregates

and microaggregates, and other debris. From the filter, the blood is usually returned directly to the vascular system of the patient. Ancillary circuits, typically including one to three
5 additional pumps and a small reservoir, may be used to salvage blood from the operative site. The salvaged blood is delivered to a cardiectomy reservoir where it can be filtered and stored until the surgeon returns the blood directly or indirectly
10 through the oxygenator to the patient's cardiovascular system. By these means, the requirement for external blood replacement is often minimized.

The technological improvements noted above have
15 focused on minimizing red cell damage in both the main circuit, comprising the oxygenator, arterial pump, and filter, and the ancillary blood salvage circuits. However, the presence of these devices, which are necessary for the transport and gas
20 exchange of the blood but nonetheless are foreign to the patient's body, may have a deleterious effect on leucocytes, or white blood cells, in the blood. Contact between the internal surfaces of these foreign devices and the leucocytes may elicit an
25 immune response and/or may result in the formation and release of a host of toxic mediators, and what is commonly referred to as oxygen-free radicals.

Leucocytes are a type of blood cell in the immune system which constitute the principal means
30 of defense against antigens, such as infection by pathogenic microorganisms and viruses, and probably also against most cells that undergo transformation into cancer cells. Leucocyte activation, the leucocytic monitoring and arming functions, proceeds
35 from a complex series of biochemical interactions,

typically terminating in engulfing and digesting the antigen. If the leucocytes have been so activated, but lack an appropriate antigenic target, the leucocytes may inflict damage to internal organs, particularly ischemic tissues, i.e., tissues in which no blood is flowing such as the heart and lungs during certain surgical procedures. This effect, called "reperfusion injury", is well known and is commonly caused by leucocyte activation as a result of leucocyte contact with foreign matter such as the large internal surface area of an extracorporeal circuit.

The activated leucocytes associated with reperfusion injury release both proteolytic enzymes, which may lead to the destruction of cellular function and structure, and oxygen metabolites ("free radicals") which could lead to death. Extracorporeal circuit-induced activated leucocytes have been implicated in microcirculatory stasis, leucocyte sequestration, vasospasm, organ destruction, interstitial edema, microvascular occlusion (including myofibrillar necrosis, mitochondrial disruption, and nuclear chromatin clumping), lung endothelium damage, and the release of chemotactic factors.

Leucocytes have also been implicated as the singular cause or a major contributory factor in a growing number of transfusion complications, including non-hemolytic febrile reactions, alloimmunization, viral transmission (e.g., Cytomegalovirus, Human T-cell Lymphotropic Virus Type I), immune suppression and modulation, graft versus host reactivity, and refractoriness to platelets. Moreover, with increasing frequency, the most common leucocyte, the granulocytic neutrophil,

has been implicated as the mediator of tissue destructive events in a variety of disorders, including reperfusion injury, respiratory distress syndromes, rheumatoid arthritis, skin disorders and ulcerative colitis. The commonality which pervades these pathologies is the neutrophil's ability to release a number of agents which can disrupt and destroy normal cellular function, dissolve connective tissue, and cause injury to organs.

It has also been shown that circulating leucocytes contribute to or mediate ischemic and reperfusion injury during organ preservation, particularly following extended preservation of the heart-lung bloc commonly required during cardiopulmonary bypass operations (CPB). Leucocytes have also been associated with increased oxygen radical activity, pulmonary edema, and vasoconstriction.

According to the present invention, a filter assembly for removing leucocytes and other deleterious matter from a liquid, such as blood, generally comprises a housing and a fibrous depth filter. The housing has an inlet and an outlet and defines a liquid flow path between the inlet and the outlet. The fibrous depth filter is positioned inside the housing across the liquid flow path and includes a fibrous structure for decreasing the leucocyte content of the liquid at a flow rate greater than about 25 milliliters per minute.

Filter assemblies which embody the invention may include a filter element having one or more of the following characteristics: a hollow, generally cylindrical configuration; an upstream portion which has a larger pore size than the downstream portion; a total fibrous surface area greater than about 2

square meters and a critical wetting surface tension (CWST) of 53 dynes per centimeter or more. The filter assemblies may have a total hold-up volume in the range from 70 cubic centimeters to 400 cubic centimeters and may further comprise a porous degassing element for removing gas from the liquid, a liquophobic membrane which allows gas but not liquid to escape from the housing, and a vent for removing gas from the housing.

10 The present invention also provides a method for removing leucocytes and other deleterious matter from a liquid, such as blood. The method generally comprises decreasing the leucocyte content of the liquid by passing the liquid through a fibrous depth filter. Methods embodying the invention may include passing the liquid through a fibrous depth filter having one or more of the following characteristics: a hollow, generally cylindrical configuration; an upstream portion which has a larger pore size than
20 the downstream portion; a total fibrous surface area greater than about 1 square meter; and a CWST of 53 dynes per centimeter or more. The method may further comprise holding up no less than 70 cubic centimeters and no more than 400 cubic centimeters
25 of the liquid; repeatedly recirculating blood through a housing in an extracorporeal circuit; separating gas from the liquid; or venting the gas from the housing.

30 Filter assemblies and methods embodying the present invention are particularly advantageous. First, they remove leucocytes very effectively. Leucocytes are not only trapped in the interstices of the fibrous depth filter but they also adhere to the surfaces of the fibers in the depth filter.
35 When the filter has a total fibrous surface area

greater than about 2 square meters, the filter most desirably provides ample surface area on which the leucocytes can adhere. When the filter has a CWST of 53 dynes per centimeter or greater, the filter is enabled most desirably to have a CWST greater than the surface tension of the liquid, allowing the liquid to readily wet the fibrous depth filter, actively seep into all of the interstices of the filter element, and completely contact the ample surface area of the fibers

Further, filter assemblies and methods embodying the present invention are capable of removing leucocytes while maintaining a large flow of liquid through the fibrous depth filter for a considerable span of time without clogging or plugging. Conventional filters may remove leucocytes at low flows, e.g., 5-10 milliliters per minute, but embodiments of the present invention are capable of removing leucocytes at much greater flow rates, even hundreds of times greater. As noted previously, because the CWST of the fibrous depth filter can be 53 dynes per centimeter or greater and, therefore, can be greater than the surface tension of the liquid, the liquid flows through the depth filter with minimal resistance due to the effects of surface tension. In addition, because the fibrous depth filter can have a hollow, cylindrical configuration and an upstream region with a larger pore size than the downstream region, the depth filter resists clogging or plugging. The hollow, cylindrical configuration presents a large surface area to liquid flowing outside-in through the depth filter and, therefore, spreads contaminants more thinly around the filter. When the upstream region has larger pores this most desirably allows the smaller contaminants to penetrate deeper into the _____

depth filter rather than accumulate on the surface of the filter to block liquid flow. Thus, although embodiments of the present invention are nonetheless effective at low flow rates, they are capable of removing leucocytes at very large flow rates for extended periods of time. For example, leucocytes may be removed from a liquid such as blood at a flow rate up to six liters per minute for three to four hours and, in some cases up to ten hours, without clogging or plugging.

While filter assemblies and methods embodying the present invention are capable of maintaining a large flow rate, they hold up very little of the liquid when flow ceases. In many situations, the liquid being filtered is whole blood obtained directly from a patient. For example, during a surgical operation or during autologous transfusion, blood can be removed from the patient and circulated through an extracorporeal circuit which includes a filter assembly of the present invention, and then returned to the patient. When the operation is completed and flow through the extracorporeal circuit ceases, the blood which remains in the extracorporeal circuit, in particular, in the filter assembly, cannot be returned to the patient. Filter assemblies embodying the present invention hold up so little blood that only about 70 cubic centimeters to about 400 cubic centimeters remain in the filter assembly after flow ceases even though the flow rate during the operation can be as high as six liters per minute.

Filter assemblies and methods embodying the present invention have a wide variety of uses. For example, a filter assembly may be used to remove leucocytes and other deleterious matter from blood

passing through it, while simultaneously allowing other blood components, such as red cells and platelets, to be returned undamaged to the patient.

5 A filter assembly or method embodying the present invention may be used in an extracorporeal circuit, such as is described above, and/or may be employed for therapeutic applications, including but not limited to autologous transfusion, leucopheresis, apheresis, or dialysis. Thus, the
10 device and method have application whenever blood or a leucocyte-containing liquid is brought into contact with external circuitry, and thence returned to the body or specific organs.

A filter assembly or method embodying the
15 present invention may also be used for cardioplegia or coronary perfusion in order to perfuse and maintain safe levels of metabolic activity within tissues and organs. Moreover, the filter assembly or method can be used for myocardial infarcted
20 patients to reduce subsequent damage during reperfusion in the affected heart region.

In addition, a filter assembly in accordance with the present invention can be used in cytoreductive therapy or in any therapeutic or
25 clinical regimen in which leucocyte depletion is beneficial. For example, certain hematological disorders result in a marked increase in blood viscosity due to a high number of circulating leucocytes. This phenomenon, called leukostasis,
30 can result in tissue and organ damage. Extracorporeal circulation of blood through a device in accordance with the present invention can be used to reduce the leucocyte count, thus reducing blood viscosity.

35 Also, as noted above, leucocyte depletion has

been successful in reducing or eliminating the deleterious effects attributed to a wide variety of injuries, diseases, or conditions. Passing the patient's blood through a device in accordance with the present invention can be used in clinical or therapeutic regimens in which leucocyte depletion is beneficial.

FIG. 1 is a sectional side view of an exemplary filtering apparatus embodying the present invention.

FIG. 2 is a partial cut away top view of the filtering apparatus of FIG. 1.

FIG. 3 is an illustration of a liquid filtering system incorporating the filtering apparatus of FIG. 1.

The present invention provides for a leucocyte depletion filter assembly for removing leucocytes and other deleterious matter from a leucocyte-containing liquid, the filter assembly comprising: (a) a housing having an inlet and an outlet and defining a liquid flow path between the inlet and the outlet; and (b) a fibrous depth filter positioned inside the housing across the liquid flow path and including a fibrous means for decreasing the leucocyte content of the liquid at a flow rate greater than 25 milliliters per minute.

The present invention also provides for a leucocyte depletion filter assembly for removing leucocytes and other deleterious matter from a leucocyte-containing liquid, the filter assembly comprising: (a) a housing having an inlet, an outlet, and a vent and defining a liquid flow path between the inlet and the outlet; (b) a degassing mechanism communicating with the vent for removing gas from the liquid; and (c) a depth filter positioned in the housing across the liquid flow

path.

The present invention further provides for a leucocyte depletion filter assembly for removing leucocytes and other deleterious matter from a leucocyte-containing liquid, the filter assembly comprising: (a) a generally cylindrical housing having first and second chambers, an inlet which allows tangential inflow into the first chamber, an outlet which allows outflow from the second chamber, and a vent; (b) a porous degassing element positioned between the first and second chambers to remove gas from the liquid; (c) a liquophobic membrane covering the vent and communicating with the degassing element to allow gas but not the liquid to flow through the vent; and (d) a hollow, cylindrical filter element positioned in the second chamber and comprising a mass of microfibers having a CWST of 52 dynes/cm or greater and a graded pore size over at least a substantial radial portion of the microfibrinous mass, the interior of the hollow filter element communicating with the outlet.

The present invention further provides for a method for removing leucocytes and other deleterious matter from a leucocyte-containing liquid comprising passing at least 25 milliliters per minute of the liquid through a fibrous depth filter.

The present invention also provides for a method for removing leucocytes and other deleterious matter from a leucocyte-containing liquid comprising: (a) directing the liquid through a housing; (b) separating gas from the liquid; (c) venting the gas from the housing; and (d) passing the liquid through a fibrous depth filter positioned within the housing, thereby decreasing the leucocyte content of the liquid.

The present invention also provides for a method of treating blood in an extracorporeal circuit comprising: (a) repeatedly circulating the blood through a housing; (b) separating gas from the blood; (c) venting the gas from the housing; and (d) passing the blood through a fibrous depth filter positioned within the housing, thereby decreasing the leucocyte content of the blood.

The present invention also provides for a method of treating blood in an extracorporeal circuit comprising: (a) directing the blood through a housing; (b) separating gas from the blood; (c) venting the gas from the housing; and (d) passing the blood through a fibrous depth filter positioned within the housing, thereby decreasing the leucocyte content of the blood.

The present invention also provides for a method for removing leucocytes and other deleterious matter from a leucocyte-containing liquid comprising: (a) directing the liquid through a fibrous depth filter at a flow rate of up to six liters per minute, and (b) removing a clinically or therapeutically significant amount of leucocytes from the liquid.

The present invention also provides for a method of treating blood in an extracorporeal circuit comprising: (a) repeatedly circulating the blood through a fibrous depth filter at a flow rate of up to six liters per minute; and (b) removing a clinically or therapeutically significant amount of leucocytes from the liquid.

A filter assembly in accordance with the present invention comprises a housing, having an inlet and an outlet, and a filter element disposed in the housing for decreasing the leucocyte content

and removing other deleterious matter from a leucocyte-containing liquid. Leucocyte-containing liquid, as used herein, refers to blood, including whole blood, treated blood, such as blood diluted
5 with a physiological solution, and one or more blood components, such as plasma or packed red cells, as well as other leucocyte- or leucocyte precursor cell-containing liquids. Deleterious matter, as used herein, includes activated and non-activated
10 leucocytes, fat emboli, microaggregates, and other debris. Preferred embodiments of the invention may also comprise a degassing mechanism cooperatively arranged with the housing for removing gaseous emboli from the liquid.

15 The filter assembly may be configured in a variety of ways in accordance with the invention. For example, the filter assembly may include a solid filter element which may have a disk-like or cylindrical shape and may be positioned in a housing
20 to filter liquid flowing longitudinally or axially through the filter element. The inlet and outlet of the filter assembly would then communicate with opposite ends of the filter element and the side of the filter element would be sealed against the
25 housing to prevent bypass of the liquid around the filter element.

Alternatively, the filter assembly may include a hollow filter element which may have a cylindrical shape and may be disposed in the housing to filter
30 liquid flowing laterally or radially through the filter element. For example, to filter liquid flowing inside/out through the filter element, the inlet and outlet of the filter assembly would be arranged to respectively communicate with the
35 interior and exterior of the hollow filter element.

In the illustrated embodiment, the filter assembly is arranged to filter liquid flowing outside/in through the filter element. This arrangement is preferred because it provides a
5 filter element with a large surface area in a compact housing.

Any housing of suitable shape to provide an inlet and an outlet for liquid and a space for a filter element disposed between the inlet and outlet
10 can be employed. A preferred embodiment of the filter assembly comprises a generally cylindrical housing 10 having an inlet 11 and an outlet 12, as shown in Figures 1 and 2. Housings can be designed to accept a variety of shapes of filter assemblies.
15 For example, a square or octagon shaped housing and other possible forms designed to accommodate a similarly shaped filter element would in principle all be functional, provided that adequate flow area is provided by the filter element. These shapes are
20 within the scope of the claimed invention.

Any housing of suitable configuration to reliably contain the liquid and define a liquid flow path through the filter element can be employed. A preferred embodiment of the filter assembly
25 comprises a housing 10 which generally includes two parts, a body 13 and a cover 14, and defines upper and lower chambers 15, 16. The cover 14 has a shallow, generally cylindrical configuration and includes a generally flat top wall 20 and a
30 downturned, generally cylindrical side wall 21.

In a preferred embodiment, the cover 14 includes the inlet 11, as shown in Figure 2. The inlet 11 may be variously configured. For example, the inlet 11 may comprise a nipple 23 which defines

an inlet passage 22 and may be molded integrally with the cover 14. In the illustrated embodiment, the inlet 11 is configured to receive the end of a tube (not shown). In a preferred embodiment, the
5 inlet passage 22 is horizontal and opens through the side wall 21 of the cover 14 in a direction tangential to the side wall 21.

The cover 14 may also be provided with an accessory port 27 and an annular baffle 24. The
10 accessory port 27 may be used to provide pressure measurements or samples of the liquid being filtered. When it is not in use, the accessory port 27 may be capped. The annular baffle 24 is preferably concentric with and spaced inwardly from
15 the side wall 21. The baffle 24 may be formed integrally with the cover 14, extending downwardly from the top wall 20, and may be generally coextensive with the side wall 21, forming a circular channel portion 25 in the upper chamber 15.
20 An opening 26 in the baffle 24 allows the circular channel 25 to communicate with a vent in the cover 14.

The vent allows gas to escape from the housing and may be configured in a variety of ways. For
25 example, it may comprise a nipple with a manually operable valve. However, in a preferred embodiment, the vent comprises one or more holes 30 spaced around the top wall 20 of the cover 14. A porous, liquophobic membrane 31 may cover the holes 30
30 allowing gas but not liquid to escape from the housing. In a preferred embodiment, the liquophobic membrane may be attached to the underside of the top wall 20 of the cover 14 to allow a relatively free flow of gas from the housing. The liquophobic
35 membrane may be variously configured. For example,

it may comprise a polytetrafluoroethylene membrane having an absolute pore rating of about 0.2μ and a polypropylene backing as a support.

5 The cover 14 and the body 13 may be joined in any suitable manner. For example, the lower end of the cover side wall 21 may include an annular channel 32 formed in a flange 33 which is configured to receive the open upper end of the body 13. The cover 14 and the body 13 may then be joined at the
10 channel 32, preferably by bonding or by welding, including spin welding or ultrasonic welding.

The body 13 includes bottom and side walls 34, 35 and may be substantially coextensive in depth with the height of the filter element 36. In a
15 preferred embodiment the side wall 35 of the body 13 generally has a smaller outer diameter than the side wall 21 of the cover 14 but flares at the upper end to provide an inclined shoulder 40.

In a preferred embodiment, the body 13 includes
20 the outlet 12. The outlet 12 may be variously configured. For example, the outlet 12 may comprise a nipple 41 which defines an outlet passage 42 and may be molded integrally with the body 13. In the illustrated embodiment, the nipple 41 projects
25 axially down from a boss 43 in the center on the underside of the bottom wall 34 and is configured to receive the end of a tube (not shown). An annular groove 44 in the inside of the boss receives an annular extension 45 which surrounds an extension 46
30 of the nipple 41 and which centrally locates the filter element 36 in the body 13.

The housing may be fabricated from any sufficiently rigid, impervious material which is compatible with the leucocyte-containing liquid.
35 For example, the housing may be fabricated from a

metal, such as stainless steel, or from a polymer. In a preferred embodiment, the housing is fabricated from a plastic material, such as polystyrene, polycarbonate, or polypropylene. In addition, all
5 of the surfaces of the housing which contact the liquid are preferably liquophilic, i.e., readily wettable by the liquid. For example, the internal surfaces of the body 13 and the cover 14 may be treated to achieve a high degree of liquophilicity,
10 e.g., by surface graft co-polymerization of hydroxyl functional monomers. These liquophilic internal surfaces then readily facilitate the release of gas bubbles during the prep and priming operation. A method of reducing the adhesion of bubbles in
15 medical equipment is disclosed in U.S. Patent 4,861,617.

The degassing element may be fashioned from any material which causes small gas bubbles in the liquid to coalesce and separate from the liquid. In
20 a preferred embodiment, the degassing element is a porous structure such as a porous foam or sponge material. In addition, the degassing element may be treated with an anti-foaming agent to aid in breaking down the film between bubbles, for example,
25 a compound of silicone and silica, such as Medical Antifoam A, available from Dow Corning Mfg. Co.

The degassing element may have any suitable configuration, preferably geometrically similar to the shape of the housing, and is preferably
30 positioned in the housing between the inlet and the filter element. For example, in the illustrated embodiment, the degassing element comprises an annular sponge 50 interposed between the upper and lower chambers 15, 16. The annular sponge 50 may be

located in the housing 10 by an annular, perforated ring 51 which preferably constitutes, in effect, an axial extension of the baffle 24. The inclined shoulder 40 holds the annular sponge 50 and
5 perforated ring 51 in place in the flared portion of the housing body 13.

The illustrated embodiment of the filter assembly includes a degassing element 50 as well as a housing 10 having a tangential inlet 11 and a vent
10 30, all for removing gas from the liquid before the liquid contacts the filter element 36. Of course, the gas may be removed from the liquid by a separate device before the liquid enters the filter assembly. The filter assembly then need not include a
15 degassing element, a tangential inlet, or a vent. The housing may then simply be only slightly larger than the filter element.

In accordance with one aspect of the invention, the filter element may be fashioned to decrease the
20 leucocyte content of a leucocyte-containing liquid which is passed through the filter element. The filter element may be fashioned in a variety of ways to effectively remove the leucocytes, as well as other deleterious matter from the liquid. For
25 example, the filter element preferably comprises a depth filter. The depth filter may preferably comprise a mass of fibers, such as a mass of microfibers. The fibers may be made from any material compatible with the liquid and may be
30 untreated or may be treated in a variety of ways to make the filter element even more effective. The fibers may be bonded, fused, or otherwise fixed to one another or they may simply be mechanically entwined.

The fiber diameters and/or the void spaces between the fibers may have a substantially constant size along the dimensions of the filter element or they may vary in a continuous or stepwise manner.

5 Further, the filter element may be configured as a flat sheet, a corrugated sheet, a solid body such as a disk or cylinder, or a hollow body such as a hollow cylinder and may include additional structures such as end caps, edge seals, a cage, a
10 core, or a wrap.

As shown in Figure 1, a preferred embodiment of the filter element 36 has a hollow, generally cylindrical configuration and comprises a wrap 52, a fibrous mass 53, a porous element 54, a perforated
15 core 55, an upper blind end cap 56, and a lower open end cap 57. The filter element 36 is preferably disposed within the lower chamber 16 in the housing 10 and is smaller in diameter than the side wall 35 of the body 13 so that an annular space 60 is left
20 between the side wall 35 and the filter element 36. The interior of the filter element 36 communicates with the centrally located outlet 12.

The wrap 52 surrounds the fibrous mass 53 and serves to protect the fibrous mass 53 from damage
25 when the filter element 36 is assembled. The wrap 52 may comprise any sufficiently flexible, porous material, preferably having a relatively large pore size. For example, the wrap 52 may be a sheet of spun-bonded, non-woven, polypropylene fibers.

30 The porous element 54, which preferably has a pore size no greater than about 40 microns, is disposed coaxially adjacent to the downstream surface of the fibrous mass 53, e.g., around the interior of the fibrous mass 53. The porous element
35 54 may be fashioned from any compatible porous

membrane or woven or non-woven material, including a mesh or a screen. The porous element 54 serves principally as a final filter to remove, for example, any aggregates which escape the fibrous mass 53 or form at the downstream portion of the fibrous mass 53.

The perforated core 55 is disposed within and adjacent to the interior of the porous element 54 and serves principally to support the fibrous mass 53 and the porous element 54 against the differential pressure across the filter element 36. Consequently, the perforated core 55 may be fashioned from any suitably rigid material including a metal such as stainless steel or a rigid polymer such as polyolefin, polyester, or polyacrylate.

The end caps 56, 57 serve to direct the liquid radially outside/in through the filter element 36. Both end caps 56, 57 are preferably fashioned from an impervious polymer, such as polypropylene, and are fixed to the respective ends of the fibrous mass 53, the porous element 54, and the perforated core 55. Alternatively, the lower ends of the fibrous mass, the porous element, and the perforated core may be fixed directly to the bottom wall of the body, eliminating the need for a lower end cap.

Alternatively, the filter element may be designed for inside/out flow. The porous element may then be disposed around the exterior of the fibrous mass, the upper end cap may be an open end cap, and the lower end cap may be a blind end cap. The core may be omitted but a cage disposed coaxially around the porous element to support the fibrous mass and the porous element against the pressure drop may be added. Of course, the housing would be rearranged to permit the inlet to

communicate with the interior of the filter element and the outlet to communicate with the exterior of the filter element.

The fibrous mass 53 may preferably be
5 configured as a mass of non-woven, synthetic,
polymeric fibers. The fibers may be bonded, fused,
or otherwise fixed to one another, or they may be
substantially free of fiber-to-fiber bonding and
10 secured to each other by mechanical entanglement or
intertwining. The term "fibers" includes filaments,
and the term "substantially free of fiber-to-fiber
bonding", as used herein, refers to the
characteristics of the fibers making up the fibrous
mass 53. Thus, although the fibrous mass 53 may
15 display random fiber-to-fiber bonding, such bonding
would not contribute in any material way to the
structural integrity of the filter element. A
preferred fibrous mass 53 is available from Pall
Corporation under the registered trademark Profile.

20 Polymeric materials particularly well suited
for the fibrous mass 53 include, but are not limited
to thermoplastics such as the polyolefins,
particularly polypropylene and polymethylpentene;
polyamides, particularly nylon 6, nylon 610, nylon
25 10, nylon 11, nylon 12; and polyesters, particularly
polybutylene terephthalate and polyethylene
terephthalate. Other suitable, but less preferred,
polymers are addition polymers such as polyvinyl
fluoride, polyvinylidene fluoride and their
30 copolymers. The preferred material is polybutylene
terephthalate.

The fibrous mass 53 may be produced by melt
blowing, in which molten resin is attenuated into
fibers by a high velocity stream of gas and

collected as a non-woven web. As disclosed in U.S. Patent No. 4,726,901, of the above noted materials, some are better adapted to melt blowing of fine fibers than are others. Material which are particularly suited to melt blowing include polyethylene, polypropylene, polymethylpentene, Nylon 6, polyester PET (polyethylene terephthalate), and polyester PBT (polybutylene terephthalate). Others that have not yet been tested may be found. Of the above listed resins, polyester PBT is a preferred material because it also lends itself to radiation grafting.

For some applications it may be desirable to form the fibrous mass 53 directly on a mandrel without the use of an internal support or core. For most purposes, however, it is desirable that the structure be able to withstand, without collapse or loss of integrity, differential pressures in the range from 0.5 psid to 175 psid, preferably in the range from 0.5 psid to 135 psid. Accordingly, for most applications, it is desirable to form the fibrous mass 53, preferably by depositing melt-blown fibers, on a hollow foraminous, or open, relatively rigid central support member or core 55 after the porous element 54 has been mounted to the core 55.

The fiber diameters may be substantially constant throughout the fibrous mass 53. Alternatively, the fiber diameters can be varied in a continuous or step-wise manner from one part of the fibrous mass 53 to another as measured in the radial direction by varying the resin and fiberizing air flow rates. Without intending to be held to a specific theory, a combination of adsorption and mechanical entrapment of leucocytes on fiber surfaces is believed to be the mechanism for

removing the leucocytes from a leucocyte-containing liquid. Since the surface area of a given weight of fibers is inversely related to the diameter of the fibers, it is to be expected that finer fibers will have higher capacity and that the quantity of fibers, as measured by weight of fibers necessary to achieve a desired efficiency, will be less if the fibers used are smaller in diameter. Fiber diameters as small as 1.5 to 2 micrometers or less may be used to fashion the fibrous mass 53.

The fibrous mass 53 also preferably has a substantially constant voids volume, typically in the range of from 60 to 95 percent, more preferably from 64 to 93 percent and even more preferably from 75 to 85 percent. When the fibrous mass 53 comprises polybutylene terephthalate (PBT) fibers, the most preferred voids volume is about 85 percent. The voids volume can be maintained substantially constant by varying the forming roll bias force on the cylindrical mass of fibers 53 as the structure is formed on the rotating porous element 54 and core 55.

The removal rating can vary with the fiber diameter. Thus, by varying the fiber diameter, removal rating can be varied continuously or stepwise from one part of the fibrous mass 53 to another in any desired manner in order to form a filter element 36 having a graded pore structure. For example, the fibrous mass 53 may include an upstream portion having a removal rating as large as 120 micrometers and a downstream portion having a removal rating as small as 0.5 micrometers, each at a beta equal to 5000. More preferably, the upstream portion may have a removal rating as large as 70 micrometers and the downstream portion may have a

removal rating as small as 5 micrometers, each at a beta equal to 5000. Such a fibrous mass may be embodied with an upstream portion having coarser fibers than the downstream portion.

5 In the illustrated embodiment, the annular thickness of the fibrous mass 53 is preferably in the range from 0.1 to 2 inches (2.5 mm to 5 cm), more preferably in the range from 0.4 to 0.8 inch (1.0 to 2.0 cm), and most preferably in the range
10 from 0.6 to 0.7 inch (1.5 to 1.8 cm). The outer diameter of the fibrous mass is preferably in the range from 2 to 3 inches (5 to 7.5 cm), more preferably 2.2 (5.5 cm) inches. The length of the fibrous mass 53 is preferably in the range from 2 to
15 3 inches (5 to 7.5 cm), more preferably 2.5 inches (6.4 cm).

Although the fibers of the microfibrous mass 53 may remain untreated, they are preferably treated to make them even more effective for removing
20 leucocytes and other deleterious matter. For example, the fibers may be surface modified to increase the critical wetting surface tension (CWST) of the fibers.

As disclosed in U.S. Patent No. 4,880,548, the
25 CWST of a porous medium may be determined by individually applying to its surface a series of liquids with surface tensions varying by 2 to 4 dynes/cm and observing the absorption or non-absorption of each liquid over time. The CWST of a
30 porous medium, in units of dynes/cm, is defined as the mean value of the surface tension of the liquid which is absorbed and that of the liquid of neighboring surface tension which is not absorbed within a predetermined amount of time. The absorbed

and non-absorbed values depend principally on the surface characteristics of the material from which the porous medium is made and secondarily on the pore size characteristics of the porous medium.

5 Liquids with surface tensions lower than the CWST of a porous medium will spontaneously wet the medium on contact and, if the medium has through holes, will flow through it readily. Liquids with surface tensions higher than the CWST of the porous
10 medium may not flow at all at low differential pressures and may do so unevenly at sufficiently high differential pressures to force the liquid through the porous medium. In order to achieve adequate priming of a fibrous medium with a
15 leucocyte-containing liquid such as blood, the fibrous medium preferably has a CWST in the range of 53 dynes/cm or higher. A CWST in the range from less than 53 dynes/cm to 115 dynes/cm or greater is preferred. For example, a CWST of greater than 90
20 dynes/cm is expected to provide better passage and protection of the platelets as they pass through the porous medium. Methods for increasing the CWST in the range of 53 dynes/cm or greater are disclosed in U.S. Patent 4,925,572. Methods for increasing the
25 CWST in the range of 90 dynes/cm or greater are disclosed in U.S. Patent 4,880,548.

For example, in whole blood, the cellular components are suspended in blood plasma, which typically has a surface tension of 73 dynes/cm.
30 Hence, if whole blood is placed in contact with the microfibrous mass 53, spontaneous wetting will occur if the microfibrous mass 53 has a CWST of 73 dynes/cm or higher.

The benefits conferred by modifying fibers to
35 CWST values higher than the natural CWST of

synthetic fibers include:

(a) When priming using pressures lower than the 0.2 kg/cm², for example by gravity, the time to achieve priming is significantly reduced. At 0.2 kg/cm², the reduction is, however, so small as to be difficult to measure.

(b) Fibrous media treated to convert the fiber surfaces to a particular range of CWST perform better with respect to efficiency and resistance to clogging than do fibrous media with CWST values outside of those ranges.

(c) The detrimental effects associated with non-wetting, e.g., uneven flow through the porous medium, are avoided.

(d) Devices made using unmodified synthetic fibers are recommended to be flushed with saline prior to use. This operation is sometimes undesirable since it causes blood loss due to hold-up within the complex tubing arrangement required, adds to cost, operation time, and operation complexity, and increases the probability that sterility may be lost.

Surface characteristics of a fiber can be modified by a number of methods, for example, by chemical reaction including wet or dry oxidation, by coating the surface by depositing a polymer thereon, and by grafting reactions which are activated by exposure to an energy source such as heat, a Van der Graff generator, ultraviolet light, or to various other forms of radiation. The preferred method is a grafting reaction using gamma-radiation, for example, from a cobalt source.

Radiation grafting, when carried out under appropriate conditions, has the advantage of considerable flexibility in the choice of reactants,

surfaces, and in the methods for activating the required reaction. Gamma-radiation grafting is particularly preferable because the products are very stable and have undetectably low aqueous extractable levels. Furthermore, the ability to prepare synthetic organic fibrous media having a CWST within a desired range is more readily accomplished using a gamma radiation grafting technique.

10 An exemplary radiation grafting technique employs one or more of a variety of monomers each comprising an ethylene or acrylic moiety and a second group, which can be selected from hydrophilic groups (e.g., -COOH, or -OH) or hydrophobic groups (e.g., a methyl group or saturated chains such as -CH₂CH₂CH₃). Grafting of the microfibrinous mass 53 may also be accomplished by compounds containing an ethylenically unsaturated group, such as an acrylic moiety, combined with a hydroxyl group, such as, 20 hydroxyethyl methacrylate (HEMA). Use of HEMA as the monomer contributes to a very high CWST. Analogues with similar characteristics may also be used to modify the surface characteristics of fibers.

25 Radiation grafting may increase fiber-to-fiber bonding in a fibrous medium. Consequently, a fibrous medium which exhibits little or no fiber-to-fiber bonding in an untreated state may exhibit significant fiber-to-fiber bonding after the 30 fibers have been radiation grafted to increase the CWST of the medium.

35 In a preferred embodiment of the invention, a leucocyte-containing liquid enters a filter assembly of the present invention through inlet passage 22 and into the circular channel 25 in upper chamber 15

where a generally circular liquid flow pattern is maintained by annular baffle 24 and the side wall 21 of the cover 14. This flow pattern produces a centrifugal force which causes at least some of the gas bubbles in the liquid, including any gross gas bubbles, to separate from the liquid and move inwardly and through the opening 26 in the baffle 24 into the central portion of the upper chamber 15. The gas in the liquid is then vented from the filter assembly through the holes 30 in the cover 14. In a preferred embodiment of the invention, the gas passes through a liquophobic membrane 31, which covers the holes 30 and prevents the liquid from escaping from the housing 10.

The liquid in channel 25 then passes, in a preferred embodiment, through the annular sponge 50 and the perforated ring 51 to the space 60 in the lower chamber. The degassing element 50 brakes the rotational flow of the liquid and dissipates the centrifugal forces which might otherwise tend to force gas bubbles toward the filter element 36. Also, as the liquid passes through the degassing element 50, any smaller gas bubbles remaining in the liquid coalesce into larger bubbles which, as the liquid flows through the perforations in the perforated ring 51, rise to the central portion of the upper chamber 15 and are vented from the filter assembly as noted above. Thus, the liquid which flows into the space 60 is substantially degassed.

In the embodiment of the invention characterized as "outside/in," the degassed liquid then passes from space 60 through filter element 36, and into the interior of the filter element 36. The filtered liquid then flows from the interior of the filter element and exits from the housing 10 by

passing through outlet 12.

In a preferred embodiment, the filter element 36 comprises a fibrous mass 53 having a graded pore size, e.g., one wherein the removal rating varies continuously or step-wise from a relatively large size in the upstream portion of the fibrous mass to a relatively small size in the downstream portion. It is believed that filter element 36 decreases the leucocyte content of the liquid by two mechanisms, both operating simultaneously. One mechanism is by adsorption of the leucocytes and other deleterious matter onto the fibrous surfaces. Adsorption is a function of the surface area of the fiber, which may be in turn a function of fiber diameter; adsorption may also be affected by the CWST of the fiber. The surface area required for specific uses of the filter assembly will vary according to the use. For example, in an extracorporeal circuit with a flow rate of as much as six liters/minute, the fiber surface area of the filter element is preferably in excess of two or three square meters. However, for some applications, it will be desirable to have a smaller quantity of fiber and/or fiber surface area incorporated into a significantly smaller filter assembly. An example is the "low flow" embodiment described below. Generally, the surface area of the fibers is sufficient to permit a large number of contacts between individual fibers of the fibrous mass and leucocytes and deleterious matter in the liquid.

The second possible mechanism, removal by filtration or mechanical entrapment, depends principally upon maintaining the removal rating of the filter medium within a specific range, but may be marginally affected by the fiber CWST. In a

preferred embodiment, the removal rating is preferably between 5 micrometers and 70 micrometers. The smaller the fiber diameter, the higher the surface area (per gram) and the smaller the effective pore size.

The flow rate of liquid passing through a filter assembly of the present invention can vary according to the particular use and for any given patient, but the flow rate should be maintained at a level which does not harm or destroy erythrocytes or platelets in the liquid. Embodiments of the invention may filter as little as 25 milliliters per minute or may have the capacity to filter up to 6 liters of liquid per minute, preferably 4 to 6 liters per minute, without clogging (i.e., without increasing the pressure across the filter element to above 15 psi). It should be apparent to one skilled in the art that varying the surface area, CWST, flow rate, removal rating, fiber diameter, and size of the housing may effect leucocyte removal capacity. Individually optimizing each of these parameters for a specific intended use is considered within the scope of the present invention.

The size of the filter assembly housing, the surface area of the fiber, the pore diameter, and the CWST all may affect the hold-up volume and the priming efficiency of the filter assembly. Hold-up volume refers to the amount of fluid required to obtain filtered fluid at the output end of the filter assembly. Hold-up volume also refers to the amount of fluid which remains in the filter assembly after it is taken off-line. Preferably, the hold up volume is between 70 cc and 400 cc, typically between 180 cc to 250 cc. One skilled in the art will recognize that changing the design

characteristics of the filter assembly may affect the hold-up volume. For example, increasing the size of the filter housing may increase the hold-up volume and removing the degassing element may
5 decrease the hold-up volume.

Priming efficiency refers to start-up of flow from the patient through the filter and back to the patient. An advantage of the filter assembly embodying this invention is that the priming time
10 may be below 2 minutes. A short priming period may be desirable in order to conserve nurse/technician time, but may also be a life-saving issue when quick administration is required as, for example, when serious blood loss is unexpectedly experienced
15 during surgery.

While the devices described herein are principally directed to a filter assembly having a capacity of passing up to 6 liters/minute, filter assemblies having a larger or smaller capacity can
20 be made. Included within the scope of the invention is a filter assembly designated as a "low flow" size, which has a flow rate of 3 liters/minute or less, has approximately one-third the fiber surface area and about one-half the capacity of the adult
25 device.

A filter assembly according to the present invention has the capacity for up to 10 hours of continuous removal of a clinically or therapeutically significant amount of leucocytes and
30 other deleterious matter from a leucocyte-containing liquid. However, many of the uses for which these filter assemblies are suitable do not require 10 hours of filtration. For example, a cardiac bypass operation may only require 6-8 hours; cardioplegia
35 may require only 2-4 minutes of filtration. Some

therapeutic protocols performed under emergency conditions require only 10-20 seconds of filtration, or several periodic or repeated filtrations of 10-20 seconds duration.

5 A filter assembly in accordance with the present invention is capable of decreasing the leucocyte content of the leucocyte-containing liquid. This generally means removing a therapeutically or clinically significant amount of
10 leucocytes from a leucocyte-containing liquid. "Therapeutically or clinically significant amount" refers an amount necessary to produce a beneficial effect on the patient or animal receiving the leucocyte depleted liquid. Such a beneficial effect
15 may be, for example, lessening reperfusion injury. A therapeutically or clinically significant amount can vary depending on the intended use and/or from patient to patient. For example, a therapeutically or clinically significant amount can be greater for
20 a cardiac bypass procedure than for cardioplegia. However, removal of a therapeutically or clinically significant amount can be and is routinely determined by a doctor or technician for treating a certain condition or disease as it pertains to the
25 specific patient or animal, and as it pertains to the particular application.

For example, in an extracorporeal circuit, a reference point (control) leucocyte count is obtained immediately prior to the operation. Once
30 the operation begins, however, the patient is constantly producing new leucocytes. Additionally, the number of circulating leucocytes can be increased merely through the doctor's alteration of an operative condition, e.g., adding Hespan to the
35 circulating blood or increasing the pump speed.

Furthermore, what is normal for one patient may be abnormal for another. However, when an embodiment of the invention is used in an extracorporeal circuit, the leucocyte content is decreased,
5 resulting in a therapeutically or clinically significant removal of leucocytes and demonstrably less reperfusion injury. Also, an embodiment of the invention may be used in an extracorporeal circuit whereby the leucocyte content in the circulating
10 blood achieves equilibrium, i.e., the amount of leucocytes produced by the patient is substantially offset by the removal of leucocytes using a leucocyte depletion filter assembly according to the present invention.

15 Furthermore, achieving leucocyte depletion in and of itself, in relation to the initial leucocyte count, may also be therapeutically or clinically significant. Some therapies require the removal of a certain number of leucocytes, e.g., to quickly
20 reduce a high leucocyte count to a lower one. Under these conditions, the mere reduction in leucocyte count may be therapeutically significant.

A filter assembly of the present invention may be used in any procedure, therapy, operation, or
25 environment in which the removal of activated leucocytes and deleterious matter is desirable or beneficial. Because leucocytes have the potential for becoming activated upon contact with almost anything ex-vivo, many applications exist for the
30 use of the filter assemblies of the present invention in reducing the number of activated leucocytes. While the filter assembly of the present invention is particularly suited for treating reperfusion-induced injury and/or achieving
35 leucocyte content equilibrium in an extracorporeal

system, one skilled in the art will recognize other contexts in which removal of leucocytes and other deleterious matter in a liquid is desirable.

Without intending to limit the invention thereby,
5 the following provides examples of such uses.

A filter assembly of the present invention may be used in any procedure which requires perfusion, the passage of blood or other fluid through the blood or lymph vessels of the body, using blood or
10 other fluid which has been exposed to anything ex-vivo (and therefore potentially containing activated leucocytes). For example, a filter assembly according to the present invention may be used in any of the different techniques for protecting the
15 heart during ischemia (no blood flow) to the heart. This is particularly evident in cardiac bypass operations, including but not limited to left heart bypass, femoral-femoral bypass, and aortic occlusion. Also, leucocyte depletion has been
20 implicated in the amelioration of a number of diseases or conditions, including the reduction of pulmonary injury seen after CPB. Leucocyte depletion appears to be the source of excellent cardiac and pulmonary protection.

25 Without intending to limit the invention thereby, an exemplary mode of operation for an embodiment of the invention is described by reference to an extracorporeal (EC) system used in a cardiopulmonary bypass (CPB) operation, as
30 illustrated in Figure 3, which shows the use of the same filter under different capacity requirements.

In a CPB operation, the EC system commonly comprises two loops. The first loop is a CPB circuit for bypassing the patient's heart and lungs,
35 i.e., involved in rendering the heart ischemic. The

second loop is a cardiotomy circuit for collecting blood from the operative site.

The EC system is primed by clamping the inlet and outlet tubing of filter assembly 62. The rest
5 of the circuit is then primed using the bypass circuit 66 by passing a priming fluid, such as physiological saline, through the circuit at a flow rate of 3-6 liters per minute. While maintaining this flow, the clamp near the outlet of the filter
10 assembly is partially opened, allowing the filter assembly to slowly fill with perfusate. The filling time is preferably no more than 2 minutes. When the priming fluid reaches the top of the filter, the outlet clamp is removed, then the inlet clamp is
15 removed, and finally, the bypass circuit is clamped.

Once the system is primed, blood from the cardiovascular system of the patient is channeled into the CPB circuit through tubing into an oxygenator 61 which removes carbon dioxide from the
20 blood and replaces it with oxygen. Oxygen is delivered to the oxygenator 61 through an oxygen filter 67. A pump 65 draws the oxygenated blood through a filter assembly 62 of the present invention, after which the filtered blood is
25 returned to the cardiovascular system of the patient.

In the cardiotomy circuit, excess blood from the surgical site is removed from the patient by pump 63 and delivered to a cardiotomy reservoir 64.
30 Periodically, blood is drawn (or flows by gravity) from the cardiotomy reservoir 64 into a filter assembly 68 of the present invention, and then into the oxygenator 61, where it is mixed with the blood in the CPB circuit. Filter assemblies 62 and 68 may
35 be the same type of filter assembly, or they may be

different, but both are intended to be a filter assembly according to the present invention. Thus, a filter assembly of the present invention may be used in environments which require a capacity of up
5 to 6 liters/minute, and which function at that level (for example, the CPB circuit) or at a fraction of that level (for example, the cardiectomy circuit).

In addition to the extracorporeal circuit described above, another use of the filter
10 assemblies of the present invention include arterial line filters, wherein the blood which flows through the circuit comes from a patient's artery. Typically, the pressure needed to produce throughflow is the patient's blood pressure, but it
15 may be supplemented by an in-line pump. Similar to the extracorporeal circuit noted above, arterial line filters according to the invention have the capacity to achieve leucocyte equilibrium. In use, establishing leucocyte equilibrium indicates that
20 the leucocyte count when the filter assembly is present is lower than the leucocyte count when the filter assembly is not present.

More and more, cardiopulmonary bypass, as a treatment or surgical protocol, is being extended to
25 non-cardiac applications as the knowledge concerning the pathogenic nature of leucocytes increases. All of these protocols may be improved by the inclusion of a leucocyte depletion filter of the present invention. For example, neurosurgeons use CPB in
30 operations involving the brain, the central nervous system, and for the surgical repair of aneurysms, fistulae, cerebral blood vessel anomalies, and blood clots. CPB is also used in abdominal surgery to provide a means of hypothermia and circulatory
35 arrest, and for isolating the abdominal venous

circulation. CPB may also be used in exposure hypothermia to rewarm the victim and to offset or eliminate myocardial damage. CPB is used for whole body hyperthermia in the treatment of certain
5 cancers which are sensitive to elevated temperatures. CPB may be used in isolated limb perfusion in order to eliminate or reduce the transport of toxic drugs and their side effects by compartmentalizing blood flow. An embodiment of the
10 invention may be incorporated into any of these protocols in order to achieve a clinically or therapeutically significant effect.

Leucocyte depletion using a filter assembly of the present invention may also ameliorate common
15 post-hypothermic pathologies.

In organ transplantation, the success of the transplant may depend on suppressing the body's natural tendency to rid itself of "foreign" tissue. This can be achieved through a variety of powerful
20 immunosuppressive drugs, some of which kill lymphocytes, and others of which stimulate antibodies that inactivate lymphocytes. Included within the scope of this invention are therapies which combine the use of immunosuppressive drugs and
25 filtering circulating blood to remove deleterious material from the bloodstream. In liver transplantation, massive blood loss and blood usage, as well as reducing or eliminating donor organ damage due to activated leucocytes, would benefit
30 from leucocyte depletion using a filter assembly of the present invention.

Also included within the scope of this invention is the use of a filter assembly in procedures with ischemic or ischemic-like episodes,
35 and for the reperfusion of blood for the whole body,

for regional areas, or for isolated areas.

Leucocyte depletion, and the filter assemblies of the present invention, may also be used therapeutically for conditions in which leucocytes
5 play an interactive role with vascular endothelial cells, including but not limited to Adult Respiratory Distress Syndrome, allograft rejection, shock states, coronary occlusion, and stroke.

The filter assembly of the present invention is
10 also particularly useful in therapeutic protocols involving apheresis, either alone, or in conjunction with other therapies. Leucopheresis, the selective removal of leucocytes, may be used to obtain
15 leucocyte donation or as a therapeutic measure in patients with elevated peripheral blood white cell count. A wide number of disorders, diseases and conditions may be diagnosed and/or treated using leucopheresis. The filter assemblies of the present invention may be used as or in a leucopheresis
20 apparatus.

A filter assembly of the present invention may also be used in a wide variety of therapies for treating autoimmune diseases (e.g., systemic lupus erythematosus, rheumatoid arthritis, thyroiditis,
25 myasthenia gravis, multiple sclerosis, and certain kinds of anemia). These therapies include radiation of the lymph nodes, immunosuppressive drugs developed as anti-cancer agents, and apheresis, a sort of "blood washing" that removes diseased cells
30 and harmful molecules from the circulation. For example, special leucocytes (e.g., labeled and/or killer leucocytes) have been and are being developed for the diagnosis and treatment of disorders involving neoplastic cells. A filter assembly of
35 the present invention may be used to remove these

1 special leucocytes after they have performed their
2 therapeutic or diagnostic function.

3 A filter assembly of the present invention may
4 also be used in the treatment of viral infections and
5 diseases. In the blood, viruses may be present in the
6 plasma, or may be associated with particular types of
7 leucocytes, with platelets, or with erythrocytes.
8 Leucocyte-associated viremia (the presence of a virus
9 in the bloodstream) is a feature of several types of
10 infection, including but not limited to infectious
11 mononucleosis, measles, and smallpox. Circulating
12 leucocytes are themselves a source of replicating
13 virus; viremia is usually maintained if there is a
14 continued release of the virus into the blood. For
15 example, post-transfusion mononucleosis (also known as
16 postperfusion syndrome) is a febrile condition commonly
17 seen in patients receiving massive blood transfusion
18 (e.g., for open-heart surgery). Cytomegalovirus (CMV)
19 can be isolated from the leucocytes of these patients.
20 Latent CMV infection also commonly occurs in patients
21 undergoing prolonged immunosuppressive therapy for
22 kidney transplants, leukemia, or cancer. In addition,
23 infectious mononucleosis is also is also associated
24 with Epstein-Barr Virus (EBV), typically manifested by
25 leucopenia followed by leucocytosis. Treatment of
26 these conditions may be facilitated by using a filter
27 assembly of the present invention.

28 The invention manifests itself in a number of
29 different aspects. Thus in one aspect a leucocyte
30 depletion filter assembly for removing leucocytes and
31 other deleterious matter from a leucocyte-containing
32 liquid, comprises a housing having an inlet and an

1 outlet and defining a liquid flowpath between the inlet
2 and the outlet, and a fibrous filter positioned inside
3 the housing across the liquid flowpath and including
4 fibrous means having a CWST of 52 dynes/cm or greater.

5 In another aspect of the invention a leucocyte
6 depletion filter assembly for removing leucocytes and
7 other deleterious matter from a leucocyte-containing
8 liquid, comprises a housing having an inlet and an
9 outlet and defining a liquid flowpath between the inlet
10 and the outlet, and a fibrous filter positioned inside
11 the housing across the liquidflow path and including
12 fibrous means having a graded pore structure over at
13 least a substantial portion of the flowpath.

14 In another aspect a leucocyte depletion filter
15 assembly for removing leucocytes and other deleterious
16 matter from a leucocyte-containing liquid, comprises a
17 housing having an inlet and an outlet and defining a
18 liquid flowpath between the inlet and the outlet, and a
19 fibrous filter positioned inside the housing across the
20 liquidflow path and including fibrous means having a
21 total fibrous surface area greater than two square
22 metres.

23 In another aspect a leucocyte depletion filter
24 assembly for removing leucocytes and other deleterious
25 matter from a leucocyte-containing liquid, comprises a
26 housing having an inlet and an outlet and defining a
27 liquid flowpath between the inlet and the outlet, and a
28 fibrous filter positioned inside the housing across the
29 liquidflow path and including fibrous means, the
30 assembly having a hold up volume in the range of from
31 70 to 400 cubic centimetres.

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1 In another aspect a leucocyte depletion filter
2 assembly for removing leucocytes and other deleterious
3 matter from a leucocyte-containing liquid, comprises a
4 housing having an inlet and an outlet and defining a
5 liquid flowpath between the inlet and the outlet, and a
6 fibrous filter positioned inside the housing across the
7 liquidflow path and including fibrous means, the
8 housing having a liquophobic interior surface.

9 In another aspect a leucocyte depletion filter
10 assembly for removing leucocytes and other deleterious
11 matter from a leucocyte-containing liquid, comprises a
12 housing having an inlet and an outlet and defining a
13 liquid flowpath between the inlet and the outlet, and a
14 fibrous filter positioned inside the housing across the
15 liquidflow path and including fibrous means, the
16 housing causing circular flow of the incoming feed from
17 the inlet.

18 In another aspect a leucocyte depletion filter
19 assembly for removing leucocytes and other deleterious
20 matter from a leucocyte-containing liquid, comprises a
21 housing having an inlet and an outlet and defining a
22 liquid flowpath between the inlet and the outlet, and a
23 fibrous filter positioned inside the housing across the
24 liquidflow path and including fibrous means, degassing
25 means being provided for removing gases from the liquid
26 being filtered.

27 The term depth filter, as used herein, refers to a
28 porous medium having pores capable of removing
29 particles from a fluid, the particles becoming trapped
30 by progressive interception through a tortuous pathway
31 within the structure of the medium. For example, depth
32

1 filters may include a thin fibrous membrane, pleated or
2 unpleated, as well as a thick fibrous mass, such as a
3 cylindrical mass.

4 Although the foregoing invention has been
5 described in some detail by way of illustration and
6 example, it should be understood that the invention is
7 not limited thereto, and that many obvious
8 modifications and variations thereof can be made, and
9 that such modifications are intended to fall within the
10 scope of the appended claims.

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1. A leucocyte depletion filter assembly for removing leucocytes and other deleterious matter from a leucocyte-containing liquid, the filter assembly comprising :

a housing having an inlet and an outlet and defining a liquid flowpath between the inlet and the outlet, and

a fibrous depth filter positioned inside the housing across the liquid flow path and including a fibrous means for decreasing the leucocyte content of the liquid at a flow rate greater than 25 milliliters per minute.

2. A leucocyte depletion filter assembly for removing leucocytes and other deleterious matter from a leucocyte-containing liquid, the filter assembly comprising :

a housing having an inlet, an outlet, and a vent and defining a liquid flow path between the inlet and the outlet;

a degassing mechanism communicating with the vent for removing gas from the liquid; and

a depth filter positioned in the housing across the liquid flowpath.

3. A leucocyte depletion filter assembly for removing leucocytes and other deleterious matter from a leucocyte-containing liquid, the filter assembly comprising :

1 a generally cylindrical housing having
2 first and second chambers, an inlet which allows
3 tangential inflow into the first chamber, an outlet
4 which allows outflow from the second chamber, and a
5 vent;

6 a porous degassing element positioned
7 between the first and second chambers to remove gas
8 from the liquid;

9 a liquophobic membrane covering the vent
10 and communicating with the degassing element to allow
11 gas but not the liquid to flow through the vent; and

12 a hollow, cylindrical filter element
13 positioned in the second chamber and comprising a mass
14 of microfibers having a CWST of 52 dynes/cm or greater
15 and a graded pore size over at least a substantial
16 radial portion of the microfibrous mass, the interior
17 of the hollow filter element communicating with the
18 outlet.

19

20 4. A leucocyte depletion filter assembly as
21 claimed in any one of Claims 1 to 3 having a capacity
22 of one to six liters per minute at a differential
23 pressure less than 15 psi.

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25 5. A leucocyte depletion filter assembly as
26 claimed in any one of Claims 1 to 4 having a hold up
27 volume in the range from 70 cc to 400 cc.

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29 6. A leucocyte depletion filter assembly as
30 claimed in Claim 5 having a hold up volume in the range
31 from 180 cc to 250 cc.

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1 7. A leucocyte depletion filter assembly as
2 claimed in any one of Claims 1 to 6 in which the
3 fibrous means has a graded pore structure.

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5 8. A leucocyte depletion filter assembly as
6 claimed in Claim 7 in which the fibrous means includes
7 an upstream portion and a downstream portion, the
8 upstream portion comprising generally coarser fibers
9 than the downstream portion.

10
11 9. A leucocyte depletion filter assembly as
12 claimed in any one of Claims 1 to 8 in which the
13 fibrous means has a total fibrous surface area greater
14 than two square meters.

15
16 10. A leucocyte depletion filter assembly
17 as claimed in any one of Claims 1 to 9 in which the
18 fibrous means has a hollow, generally cylindrical
19 configuration.

20
21 11. A leucocyte depletion filter assembly as
22 claimed in any one of Claims 1 to 10 in which the
23 fibrous means has a CWST of at least 52 dynes/cm.

24
25 12. A leucocyte depletion filter assembly as
26 claimed in Claim 11 in which the CWST is at least 90
27 dynes/cm.

28
29 13. A leucocyte depletion filter assembly as
30 claimed in any one of Claims 1 to 12 in which the
31 housing has a liquophobic interior surface.

32

1 14. A filter assembly as claimed in Claim 1
2 substantially as specifically described herein with
3 reference to the accompanying drawings.

4
5 15. A method for removing leucocytes and
6 other deleterious matter from a leucocyte-containing
7 liquid comprising :

8 passing at least 25 milliliters per
9 minute of the liquid through a fibrous depth filter.

10

11 16. A method for removing leucocytes and
12 other deleterious matter from a leucocyte-containing
13 liquid comprising :

14 directing the liquid through a housing;
15 separating gas from the liquid;
16 venting the gas from the housing;
17 passing the liquid through a fibrous
18 depth filter positioned with the housing, thereby
19 decreasing the leucocyte content of the liquid.

20

21 17. A method of treating blood in an
22 extracorporeal circuit comprising :

23 repeatedly circulating the blood through
24 a housing;

25 separating gas from the blood;
26 venting the gas from the housing;
27 passing the blood through a fibrous
28 depth filter positioned within the housing, thereby
29 decreasing the leucocyte content of the blood.

30

31 18. A method of treating blood in an
32 extracorporeal circuit comprising :

1 directing the blood through a housing;
2 separating gas from the blood;
3 venting the gas from the housing;
4 passing the blood through a fibrous
5 depth filter positioned within the housing, thereby
6 decreasing the leucocyte content of the blood.

7
8 19. A method for removing leucocytes and
9 other deleterious matter from aleucocyte-containing
10 liquid comprising :

11 directing the liquid through a fibrous
12 depth filter at a flow rate of up to six liters per
13 minute; and

14 removing a clinically or therapeutically
15 significant amount of leucocytes from the liquid.

16
17 20. A method of treating blood in an
18 extracorporeal circuit comprising :

19 repeatedly circulating the blood through
20 a fibrous depth filter at a flow rate of up to six
21 liters per minutes; and

22 removing a clinically or therapeutically
23 significant amount of leucocytes from the liquid.

24
25 21. A method as claimed in any one of Claims
26 15 to 20 further comprising passing 1-6 liters per
27 minute of the liquid through the fibrous depth filter.

28
29 22. A method as claimed in any of of Claims
30 15 to 21 further comprising passing the liquid through
31 a fibrous medium having a CWST of at least 52 dynes/cm.

32

1 23. A method as claimed in Claim 22 in which
2 the CWST is at least 90 dynes/cm.

3
4 24. A method as claimed in any one of Claims
5 15 to 23 further comprising holding up no less than 70
6 cc of liquid and no more than 400 cc of liquid.

7
8 25. A method as claimed in Claim 24 further
9 comprising holding up no less than 180 cc of liquid and
10 no more than 250 cc of liquid.

11
12 26. A method as claimed in any one of Claims
13 15 to 25 further comprising passing the liquid through
14 an upstream portion of the fibrous depth filter and
15 passing the liquid through a downstream portion
16 comprising finer fibers than the upstream portion.

17
18 27. A method as claimed in any one of Claims
19 15 to 26 comprising passing the liquid radially through
20 a hollow, cylindrical depth filter.

21
22 28. A method as claimed in any one of Claims
23 15 to 27 comprising passing the liquid through a
24 fibrous depth filter having a total fibrous surface
25 area of no less than two square meters.

26
27 29. A method of treating blood as claimed in
28 Claim 15 substantially as specifically described herein
29 with reference to the examples.

30
31
32